

# 复材约束海水海砂混凝土应力-应变统一模型



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# 1

## 简介

# 1 简介

- 随着对海洋资源开发的增加，海洋和沿海基础设施的需求也在大量增长。
- SSC (海水海砂混凝土，Seawater sea sand concrete) 在沿海城市和近海岛屿具有明显优势。
- 由于SSC的氯化物浓度高，钢容易被腐蚀。



# 1 简介

- 当SSC受到FRP的外部约束时，FRP可以有效减缓和抑制氯化物对混凝土的渗透，从而确保FRP-SSC结构在海洋环境中的耐久性。
- 一些学者对FRP约束SSC的轴压行为进行了研究。



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# 2

## 数据库

## 2 数据库

数据库中共361个FRP约束SSC柱的实验结果。

Shape	Literature	n	D	H	r	f <sub>c0</sub>	FRP	E <sub>frp</sub>	t <sub>frp</sub>
Circular	Zeng, 2017	117	150	300	-	23.5~36.9	BFRP CFRP	94.1, 257.1	0.15~0.30
	He, 2018	60	150	300	-	42.4~52.5	CFRP	247.0	0.17~0.33
	Yuan, 2018	120	150	300	-	28.0~39.4	BFRP CFRP	94.1, 257.1	0.15~0.30
	Yang et al. 2020	4	150	300	-	32.8	CFRP	235.0	0.17~0.33
	Zeng et al. 2020	18	150	300	-	39.1~40.6	CFRP	238.3	0.17~0.50
Square	Yang, 2018	30	150	300	0~75	34.8~36.7	CFRP	248.4	0.33
	Zeng et al. 2020	12	150	300	30	39.1~40.6	CFRP	238.3	0.17~0.50

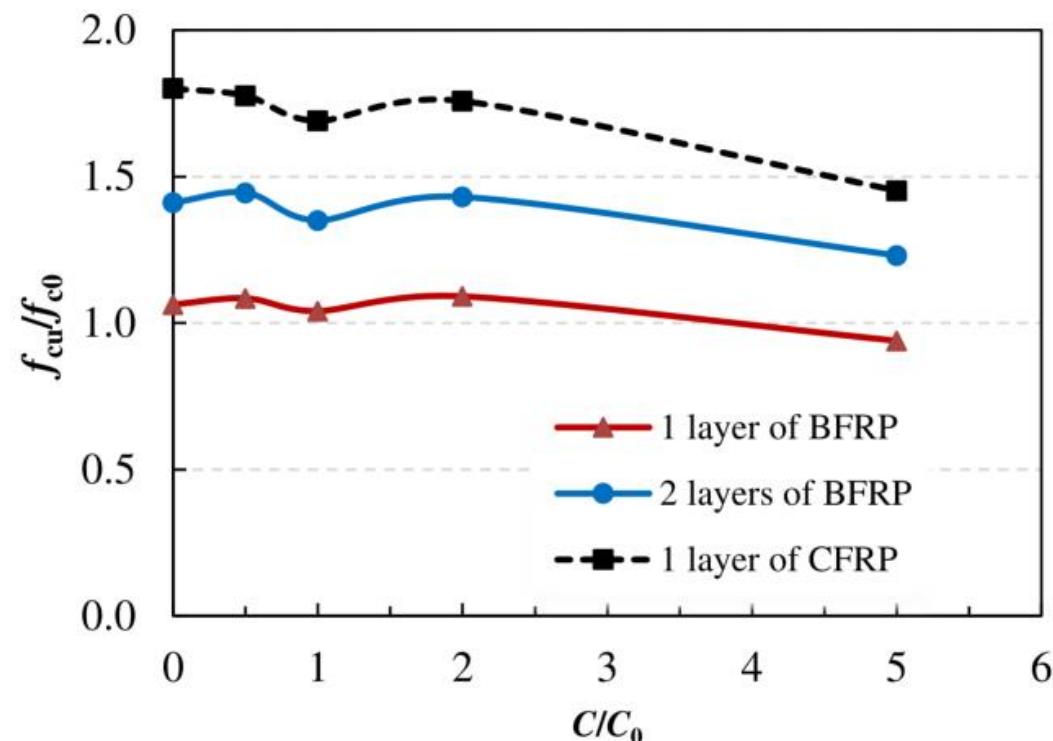


# 3

## 既有模型评价

### 3 既有模型评价

对于相同的FRP约束，普通混凝土和SSC的性能仍有差异<sup>[4]</sup>.



氯离子浓度影响

- 对于FRP约束普通混凝土，对于1层BFRP约束、2层BFRP限制和1层CFRP约束下的试样， $f_{cu}/f_{c0}$ 分别等于1.06、1.41和1.80。
- 结果表明，氯离子的存在削弱了FRP对混凝土的增强作用。

### 3既有模型评价

#### 既有模型预测性能

Model	Prediction of $f_{cu}$			Prediction of $\varepsilon_{cu}$		
	AAE [%]	M [%]	SD [%]	AAE [%]	M [%]	SD [%]
<b>Circular columns</b>						
Lam and Teng, 2003	10.0	103.0	12.6	30.2	109.8	46.4
Ozbakkaloglu and Lim, 2013	10.3	103.9	12.8	27.7	99.8	44.6
Wei and Wu, 2012	12.6	88.1	8.6	35.0	84.1	52.2
<b>Square columns</b>						
Lam and Teng, 2003	12.4	91.0	11.6	31.9	68.1	15.6
Wei and Wu, 2012	18.2	81.9	13.7	43.9	56.1	15.5
Lim and Ozbakkaloglu, 2014	16.8	83.2	10.3	14.3	91.5	21.9

$$AAE = \frac{\sum_{i=1}^n \left| \frac{Mod_i - Exp_i}{Exp_i} \right|}{n}$$

$$M = \frac{\sum_{i=1}^n Mod_i}{n}$$

$$SD = \sqrt{\frac{\sum_{i=1}^n \left( \frac{Mod_i}{Exp_i} - M \right)^2}{n - 1}}$$

# 4

## 应力-应变统一模型

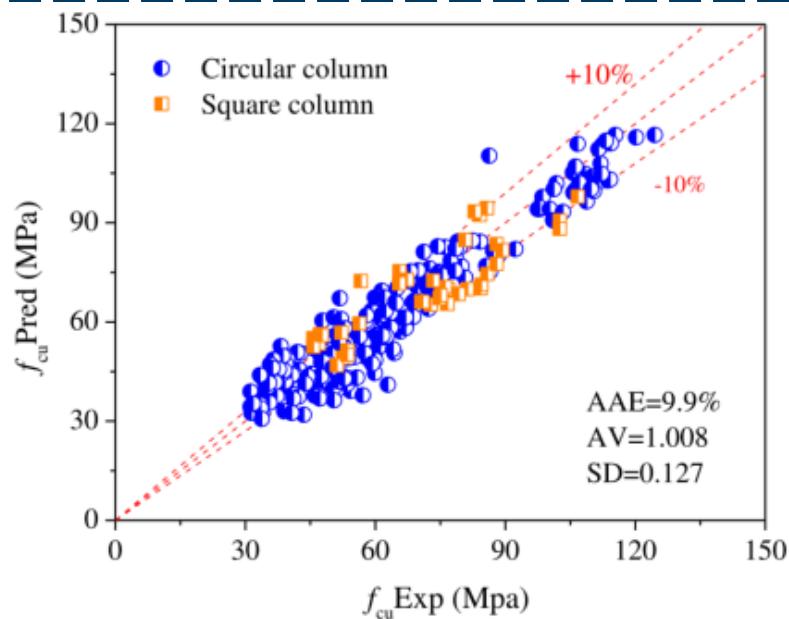
## 4 应力-应变统一模型

### 极限强度统一模型

$$\frac{f_{cu}}{f_{c0}} = 1 + k \frac{f_1}{f_{c0}} \left( a_1 + a_2 \frac{2r}{L} \right)$$

$$f_1 = \frac{2E_{frp} t_{frp} \varepsilon_{h,rup}}{L}$$

- 通过回归分析得到  $k$ ,  $a_1$  及  $a_2$  的值为 3.4, 0.52 and 0.48。



- 对于圆形柱和方形柱，极限强度统一方程获得了良好的精度，AAE、AV和SD分别等于9.9%、1.008和0.127。

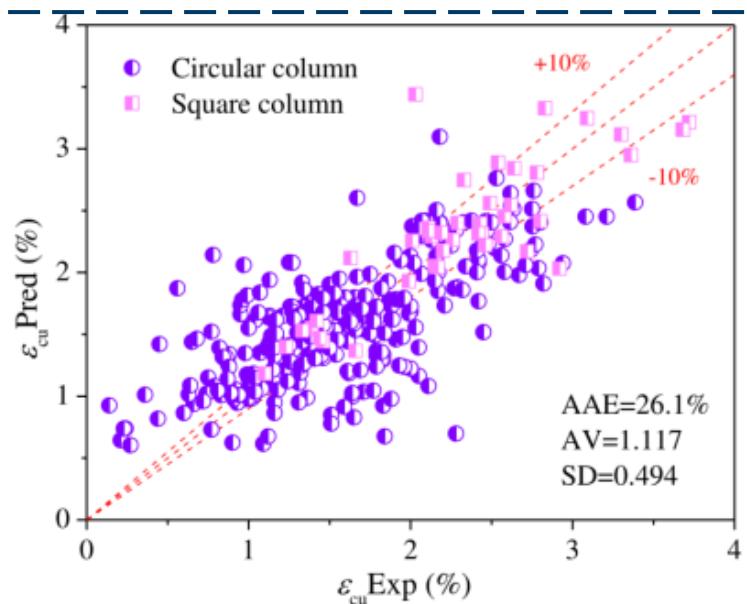
## 4 应力-应变统一模型

### 极限应变统一模型

$$\frac{\varepsilon_{cu}}{\varepsilon_{c0}} = m_1 + m_2 \left( 0.9 + 0.1 \frac{2r}{L} \right) \left( \frac{K_1}{f_{c0}} \right)^{m_3} \left( \frac{\varepsilon_{h,rup}}{\varepsilon_{c0}} \right)^{m_4}$$

$$K_1 = \frac{2E_{frp} t_{frp}}{L}$$

- 通过回归分析得到 $m_1, m_2, m_3$  及 $m_4$ 的值为3.16, 0.03, 0.9 and 1.35。



- 极限应变模型显示出更高的精度，AAE等于26.1%，AV等于1.117，SD等于0.494。

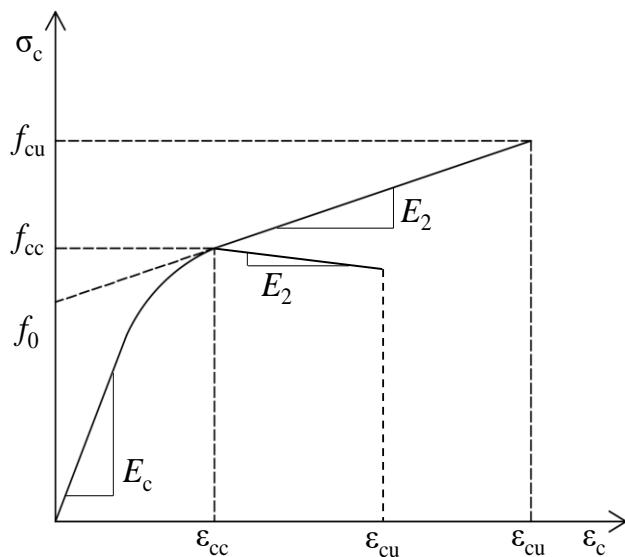
## 4 应力-应变统一模型

### 轴向应力-轴向应变统一模型

基准模型[5]:

$$\frac{\sigma_c}{f_{cc}} = \frac{ax}{a - 1 + x^{a(x+\delta)^b+c}}$$

$x = \varepsilon_c / \varepsilon_{cc}$ ;  
 $f_{cc}$ 、 $\varepsilon_{cc}$  为峰值应力及峰值应变;  
 $a, b, c$  及  $\delta$  为模型参数,  $b$  和  $\delta$  等于-0.1 及 0.01.



$$a = \frac{E_c}{E_c - \frac{\sigma_{cc}}{\varepsilon_{cc}}}$$

$E_c$  : 未约束混凝土弹性模量。

$$c = \frac{\ln\left(\frac{f_{cc}\varepsilon_{cu}a}{f_{cu}\varepsilon_{cc}} - a + 1\right)}{\ln\varepsilon_{cu} - \ln\varepsilon_{cc}} - a\left(\frac{\varepsilon_{cu}}{\varepsilon_{cc}} + \delta\right)^{-0.1}$$

## 4 应力-应变统一模型

$$f_{cc} = f_{cu} - E_2 (\varepsilon_{cu} - \varepsilon_{cc})$$

$$\varepsilon_{cc} = \frac{2f_0}{E_c - E_2} = \frac{2(f_{cu} - E_2 \varepsilon_{cu})}{E_c - E_2}$$

Only  $\varepsilon_{cu}$ 、 $f_{cu}$ 、 $E_2$   
are needed

FRP约束圆形SSC柱的 $E_2$ ：

$$E_2 = 2.82 \rho f_{c0}$$

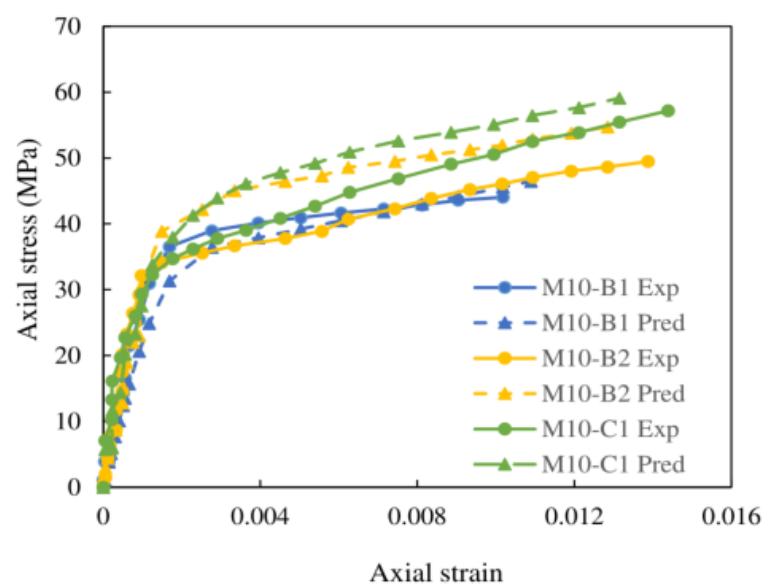
$$\rho = \frac{K_1}{f_{c0}} = \frac{2E_{frp} t_{frp}}{D f_{c0}}$$

FRP约束方形SSC柱的 $E_2$ , 考虑倒角半径:

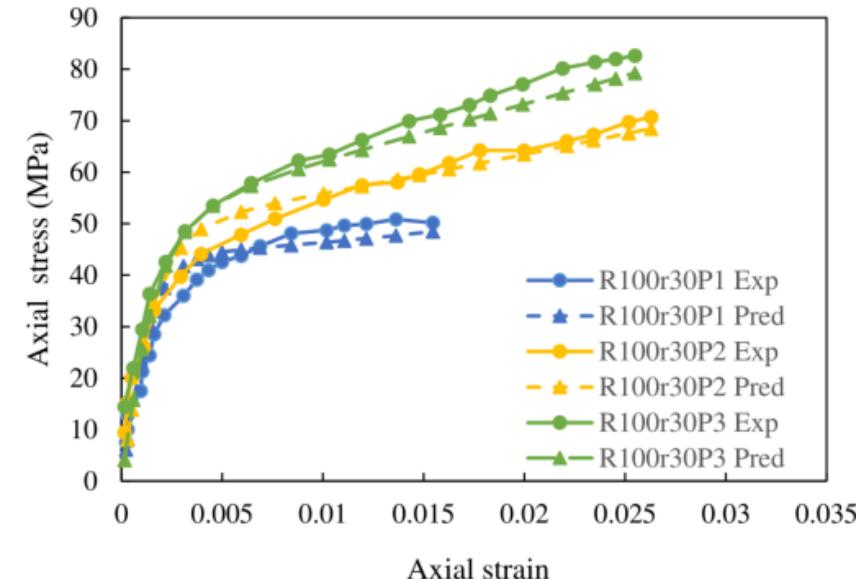
$$E_2 = 2.82 \rho f_{c0} \left( \frac{2.2r}{L} - 0.1 \right)$$

## 4 应力-应变统一模型

- FRP约束圆形和方形SSC柱统一模型的预测性能



FRP约束SSC圆柱



FRP约束SSC方柱

- 应力-应变统一模型预测精度可靠，六个试件的平均AAE、AV和SD分别等于0.18、1.00和0.28。

# 5

## 结论

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## 5 结论

- FRP约束SSC柱极限强度模型的预测精度通常高于极限应变模型。在典型的设计型模型中，Lam和Teng模型在极限应力预测精度最高，而Lim和Ozbakkaloglu模型在极限应变预测方面精度最高。
- 应力-应变统一模型通过改变参数角半径，可以同时适用于FRP约束的圆形和方形SSC柱。
- 应力-应变统一模型对FRP圆形和方形SSC柱的极限应力、极限应变和应力-应变曲线的预测结果较好。

## References

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